designideas

because of the variation in resistance you see looking into the wiper at different tap positions (**Figure 2**). At the extreme ends of the potentiometer, you see only the 400Ω wiper resistance. As the wiper moves toward midpoint, the resistance increases toward a maximum of one-quarter of the end-to-end resistance value. Because IC_1 is a 10-kΩ potentiometer, the resistance the wiper sees at midpoint is about 2.5 kΩ in series with R_{WIPER}. This variation introduces a maximum linearity error of 8%, which is negligible in most LED applications. IC_2 offers thermal protection against excessive heat and overload conditions. For effective power dissipation and to avoid thermal cycling, you must connect the exposed pad of the package to a large-area ground plane. EDN

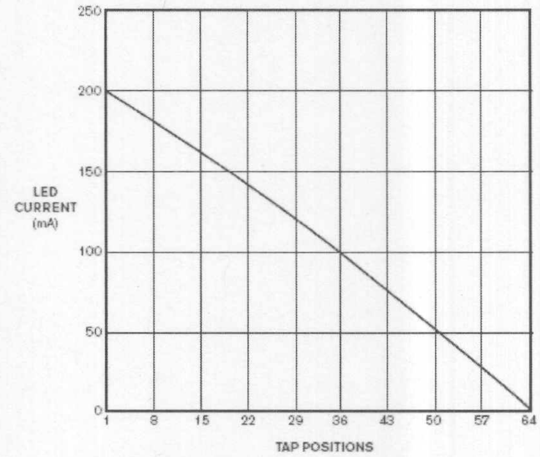

Figure 2 A plot of LED current versus tap position in Figure 1 exhibits only a slight nonlinearity.

Controlled power supply increases op amps' output-voltage range

Yakov Velikson, Lexington, MA

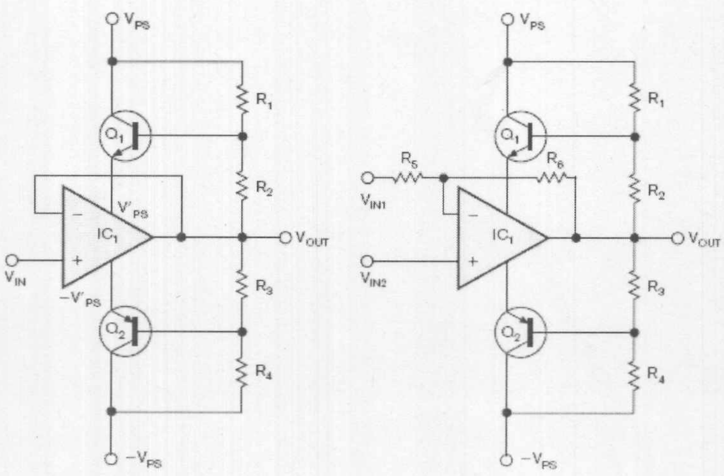

Figure 1 These simple circuits present the general methods of connecting the amplifier as an inverter or a follower to effect increased output voltage.

Increasing the output voltage of IC operational amplifiers usually involves adding high-voltage external transistors. The resulting circuit then requires correction to retain its operating characteristics. This correction is difficult, especially for precise amplifiers. This Design Idea presents an alternative: the use of a controlled power supply for the operational amplifier itself, which can increase the output voltage for many precise operational amplifiers without altering their operational characteristics. You can accomplish this task by connecting controlled transistors to the power supply of the amplifier. Resistor dividers that connect to the amplifier's output and bipolar high voltages control these transistors (**Reference 1**). The simple circuits in **Figure 1** present general methods of connecting the amplifier as an inverter or a follower to effect increased output voltage.

Dividers with resistors R_1, R_2, R_3, and R_4 determine the scale of power supply V'_{PS} and $-V'_{PS}$ for the amplifiers. If the output voltage ranges from ±22V,

resistor $R_1=R_2=R_3=R_4=R$, and V_{PS} and $-V_{PS}$ are 28V, then voltages V'_{PS} and $-V'_{PS}$ fall in the following range, allowing for any additional loss: $V'_{PS}=V_{PS}R_2/(R_1+R_2)+V_{OUT}(-V_{OUT})R_1/(R_1+R_2)$, and $-V'_{PS}=-V_{PS}R_3/(R_3+R_4)+V_{OUT}(-V_{OUT})R_4/(R_3+R_4)$ or $3V<V'_{PS}<25V$ and $-3V>-V'_{PS}>-25V$. However, power-supply circuits include transistors, which create junction resistance, affecting the amplifier's operation.

You can use supporting amplifiers to reduce losses and increase the quality of the output voltage of the primary amplifier. The requirements for supporting amplifiers are simple. They should have power supplies with opposite polarity from and lower applied voltage than that of the main power supply. They should provide the necessary power to the primary amplifier, and their frequency range should be slightly higher than that of the primary amplifier. You can use supporting amplifiers to eliminate the transitional resistances of transistors in power-supply connections. Thus, these circuits offer flexibility across a range of amplifier configurations (**references 2 and 3**).

Figure 2 shows an example of how to connect supporting amplifiers as followers. You derive output voltages V'_{PS} and $-V'_{PS}$ from resistor connections with the following equations: $V'=V_{PS1}R_7/(R_6+R_7)+V_{OUT}(-V_{OUT})R_6/(R_6+R_7)$, and $-V'=-V_{PS1}R_8/(R_8+R_9)+V_{OUT}(-V_{OUT})R_9/(R_8+R_9)$. If the supporting amplifiers have a power supply of 28V for V_{PS1} and $-2V$ for $-V_{PS2}$ for amplifier IC_2, then $-V_{PS1}=-28V$, $V_{PS2}=2V$ for amplifier IC_3, and the output voltage of amplifier IC_1, V_{OUT}, is 24V or $-24V$. Also, $R_6=R_7=R_8=R_9=R$, such that $V'=28V\times0.5+24V\times0.5=26V$. Further, $-V'=-28V\times0.5+24V\times0.5=-2V$ for $V_{OUTMAX}=24V$. $V=28V\times0.5-24V\times0.5=2V$, and $-V'=-28V\times0.5-24V\times0.5=-26V$ for $V_{OUTMIN}=-24V$. You can achieve the greatest voltage range by using separate power supplies—one for the normal voltages of the amplifier and one for the regulated part of the output voltage (**Figure 3**).

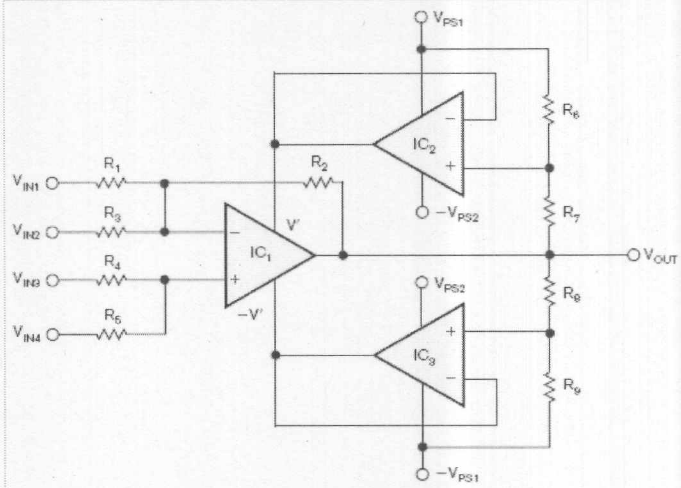

Figure 2 Replacing the transistors with op amps reduces losses and increases the quality of the output voltage of the primary amplifier.

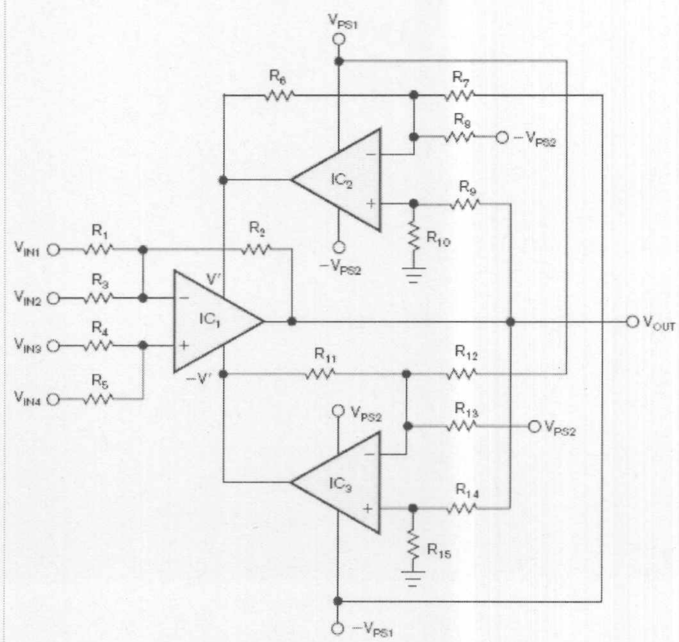

Figure 3 You can achieve the greatest voltage range by using separate power supplies–one for the normal voltages of the amplifier and one for the regulated part of the output voltage.

IC_1 is the primary amplifier. Supporting amplifiers IC_2 and IC_3 have asymmetrical power supplies. You could use many types of amplifiers in this circuit, but modern operational amplifiers may be preferable because they allow the use of the complete range of the power supply and because they handle rail-to-rail input and output. In this circuit, $V_{PS1}=28V$, $-V_{PS1}=-28V$, $V_{PS2}=2V$, and $-V_{PS2}=-2V$. The voltages of the primary amplifier are $V'=-(-V_{PS1})R_6/R_7-(-V_{PS2})R_6/R_8+(-V_{OUT})R_{10}/(R_9+R_{10})[R_7R_8+R_6(R_7+R_8)]/R_7R_8$. Further, $-V'=-(V_{PS1})R_{11}/R_{12}-(V_{PS2})R_{11}/R_{13}+(-V_{OUT})R_{15}/(R_{14}+R_{15})[R_{12}R_{13}+R_{11}(R_{12}+R_{13})]/R_{12}R_{13}$. Set $R_6=R_{10}=R_{11}=R_{15}=R$, $R_7=R_8=R_{12}=R_{13}=2R$, and $R_9=R_{14}=3R$, such that $R_6/R_7=R_6/R_8=R_{11}/R_{12}=R_{11}/R_{13}=0.5$, $R_{10}/(R_9+R_{10})=R_{15}/(R_{14}+R_{15})=0.25$, and $[R_7R_8+R_6(R_7+R_8)]/R_7R_8=[R_{12}R_{13}+R_{11}(R_{12}+R_{13})]/R_{12}R_{13}=2$. Then, substitute these values into the amplifier voltages yields $V'=14V+1V+(-V_{OUT})0.5$, and $-V'=-14V-1V+(-V_{OUT})0.5$. Minimum and maximum values for each power supply are $1.5V\leq V\leq 28.5V$, and $-1.5V\geq -V\geq -28.5V$. The total voltage of the power supply has a limit of 30V, ranging from 1.5 to 28.5V and from −1.5 to −28.5V. This range permits an increase of the output voltage of the primary amplifier by ±27V. EDN

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Single-IC-based electronic circuit replaces mechanical switch

Santosh Bhandarkar, Bangalore, India

A simple and inexpensive electronic circuit uses a low-cost pushbutton switch to toggle the electrical power on and off. The circuit replaces a more costly and bulky push-push mechanical switch. The pushbutton switch triggers a monoshot circuit. The monoshot circuit's output triggers a toggle flip-flop, which inverts its output state and controls power to the load.

Several implementations of the scheme are possible. **Figure 1** shows a single-IC implementation. The circuit uses two flip-flops, IC_1 and IC_2, in the same IC, CD4027B. You configure IC_1 as a monoshot circuit by feeding its output back to its reset pin through an RC network. IC_1 outputs a high on the rising edge of the clock by tying its J input high and its K input low. The pushbutton switch connects between the clock input of IC_1 and ground. The switch can also connect between the clock input and the positive supply, V_{DD}. By tying IC_2's J and K inputs high, IC_2 becomes a toggle flip-flop. The output of IC_1 clocks IC_2 and toggles its output on the rising edge of the IC_1 output.

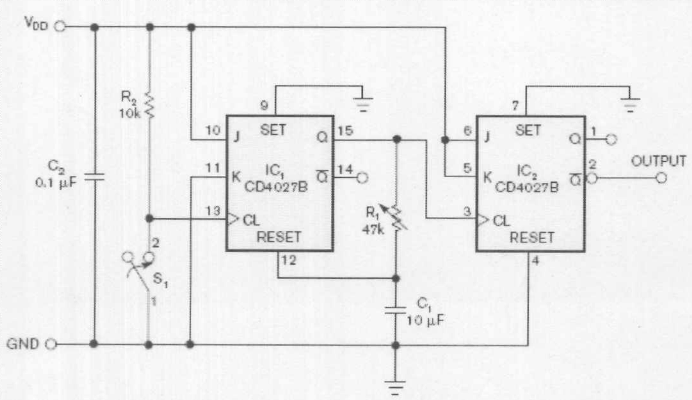

Figure 1 A pair of flip-flops configured as a monoshot and a toggle flip-flop debounce a simple, inexpensive pushbutton switch.

You can understand the operation of the circuit by observing the waveform at different points of the circuit (**Figure 2**). When you press the pushbutton switch, due to debouncing, IC_1's output goes high on the clock's rising edge. Capacitor C_1 starts charging through R_1 toward high voltage. At the same instant, IC_2 receives a rising-edge transition at its clock and toggles its output. When capacitor C_1's voltage exceeds the threshold of the IC_1 reset pin, IC_1 resets, and its output goes low. C_1 now discharges through R_1 to low voltage. The charging and discharging rate of C_1 are equal. The duration of the monoshot circuit's output pulse handles the switch-press time and the debouncing period. Varying